

# A characterization of the stochastic process underlying a stochastic Petri net

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**Abstract**— Stochastic Petri nets (SPNs) with generally distributed firing times can model a large class of systems, but simulation is the only feasible approach for their solution. We explore a hierarchy of SPN classes where modeling power is reduced in exchange for an increasingly efficient solution. Generalized stochastic Petri nets (GSPNs), deterministic and stochastic Petri nets (DSPNs), semi-Markovian stochastic Petri nets (SM-SPNs), timed Petri nets (TPNs), and generalized timed Petri nets (GTPNs) are particular entries in our hierarchy. Additional classes of SPNs for which we show how to compute an analytical solution are obtained by the method of the embedded Markov chain (DSPNs are just one example in this class) and state discretization, which we apply not only to the continuous-time case (PH-type distributions), but also to the discrete case.

**Index Terms**— Stochastic Petri nets, Markov chains, semi-Markov processes, semi-regenerative processes.

## I. INTRODUCTION

ABOUT one decade ago, Molloy [1], Natkin [2], and Symons [3] independently proposed associating exponentially distributed firing delays to the transitions of a Petri net. Generalized stochastic Petri nets (GSPNs), introduced by Ajmone Marsan, Balbo, and Conte in [4], relax this condition by allowing “immediate” transitions, with a constant zero firing time. In GSPNs, firings of immediate transitions have priority over firings of timed transitions. Each immediate transition has associated a weight which determines the firing probability in case of conflicting immediate transitions. Stochastic activity networks (SANs) [5] and stochastic reward nets (SRNs) [6] are two other classes of Petri nets where transition firing is either exponentially distributed or constant zero. GSPNs, SANs, and SRNs can be automatically transformed into continuous-time Markov chains (CTMCs) or Markov reward processes.

The need for non-exponentially distributed transition firing times in SPNs has been observed by several authors. Bechta, Geist, Nicola, and Trivedi defined extended stochastic Petri nets (ESPNs) [7], where the firing delay of timed transitions may have arbitrary distribution. The numerical solution for ESPNs

is applicable when the underlying stochastic behavior is a semi-Markov process. Ciardo proposed several extensions to ESPNs and called this modeling formalism semi-Markov SPNs (SM-SPNs) [8]. Deterministic and stochastic Petri nets (DSPNs), introduced by Ajmone Marsan and Chiola [9] as an extension to GSPNs, include exponentially distributed and constant timing. If at most one deterministic transition is enabled in a marking, the steady-state solution can be computed using an embedded Markov chain. Timed Petri nets (see [10] for a recent survey paper) and generalized timed Petri nets [11] employ a discrete time-scale for their underlying Markov process. Timed transition in TPNs and GTPNs fire in three phases and the next transition to fire is preselected according to a probability distribution.

Recently, the class of extended DSPNs has been introduced [12]. In extended DSPNs, transitions with arbitrary distributed firing times are allowed under the restriction that at most one transition with non-exponentially distributed firing time is enabled in each marking. General formulas for the steady-state solution of extended DSPNs were derived using the method of supplementary variables. In case the non-exponential distributions are piecewise specified by polynomials, an efficient numerical solution is possible. Furthermore, Choi, Kulkarni, and Trivedi introduced the class of Markov regenerative SPNs (MR-SPN) in [13], [14] which is equivalent to the class of extended DSPNs. The authors observed that the stochastic process underlying a MR-SPN is a Markov regenerative process and derived general formulas for the transient and steady-state solution. The transient solution method employs inversion of matrices containing expressions of Laplace-Stieltjes transforms and the inversion of Laplace transforms.

More general classes of SPNs have been considered by Haas and Shedler. They introduced regenerative SPNs and showed how this class of SPN can be analyzed by means of regenerative simulation [15]. They showed that, for each generalized semi-Markov process (GSMP) [16], there exists an equivalent SPN with generally distributed firing times [17] and proposed to analyze them by discrete-event simulation.

In this paper, we explore various subclasses of SPNs, obtained by imposing restrictions on the combinations of firing distributions types allowed or on the effect of a transition firing on the other enabled transitions. This leads to a hierarchy of SPN classes where modeling power is reduced in exchange for an increasingly efficient solution. GSPNs, DSPNs, SM-SPNs, TPNs, and GTPNs are particular entries in our hierarchy. Furthermore, we show that state discretization can be applied to both the continuous-time and the discrete-time case. The class of Discrete-time SPNs introduced by Molloy [18] is then ex-

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tended by allowing arbitrary discrete firing time distributions rather than only the geometric distribution.

We introduce the semi-regenerative SPNs (SR-SPNs) for which we show how to compute the steady state solution by embedding a Markov chain at appropriately defined regeneration points. The evolution of a SR-SPN between regeneration points is not restricted to be a CTMC, as for MR-SPNs and extended DSPNs. Thus, we relax the restriction that in any marking at most one timed transition with non-exponentially distributed firing delay is enabled. In Section IV, we present a SR-SPNs of a transmission line, where two deterministic transitions are concurrently enabled. In particular, we consider SR-SPNs where all transition firing distributions can be piecewise defined by polynomials multiplied by exponential expressions. This class of probability distribution is referred to as *exponential distributions* and includes the exponential as well as the constant distribution as special cases.

The paper is organized as follows. Section II defines SPNs and describes their behavior. A hierarchical classification of SPNs according to the underlying stochastic process is presented in Section III and the feasibility of their numerical solution is discussed. To illustrate the numerical solution method of SR-SPNs, a SR-SPN of a simple transmission line is analyzed in Section IV. Finally, concluding remarks are given.

## II. STOCHASTIC PETRI NETS

A *Petri net* is a directed bipartite graph in which the first set of vertices corresponds to places (drawn as circles) and the other set of vertices corresponds to transitions (drawn as bars). Places contain tokens which are drawn as dots. The set of arcs is divided into input, output and inhibitor arcs (drawn with an arrowhead on their destination, inhibitor arcs have a small circle), with each arc is associated a multiplicity. A *marking* of a Petri net is given by a vector which contains as entries the number of tokens in each place. A transition is said to be *enabled* in a marking if all of its input places contain at least as many tokens as the multiplicity of the corresponding input arc and all of its inhibitor places contain fewer tokens than the multiplicity of the corresponding inhibitor arc. A transition *fires* by removing tokens from the input places and adding tokens to the output places according to the arc multiplicities. The *reachability* set is defined to be the set of all marking reachable by firings of transitions from the initial marking.

Throughout this paper, we adopt the common formalism introduced for Petri nets in which transition firings is augmented with time [6]. We consider *stochastic Petri nets* (SPN) where the firing of a transition is an atomic operation and two types of transitions exist: *immediate transitions*, which fire without delay, and *timed transitions*, which fire after a random firing delay. The firing of immediate transitions has priority over the firing of timed transitions. Each immediate transition has associated a weight which determines its firing probability in case this transition is conflicting with some other immediate transition. The firing delay of each timed transition is specified by a probability distribution function. As a consequence, the reachability set of a SPN can be divided into *vanishing* and *tangible* markings depending on whether an immediate transition is enabled or not. The tangible markings of a SPN correspond

to the states of an underlying stochastic process, the *marking process*. Firing weights of immediate transitions, average firing delays of timed transitions, and arc multiplicities may be marking-dependent. Each quantity is evaluated in the marking *before* determining which transitions are enabled and what effect they have when they fire.

A timed transition is denoted by  $t$ , the set of all timed transitions by  $T$ . A tangible marking is denoted by  $\mu$ , the tangible reachability set by  $\mathcal{S}$ .  $\mathbf{E}(\mu)$  is the set of transitions enabled in marking  $\mu$  and  $\mathcal{S}_t = \{\mu \in \mathcal{S} \mid t \in \mathbf{E}(\mu)\}$  is the set of markings where  $t \in T$  is enabled.  $F_t(\mu, \cdot)$  is the probability distribution function for the firing time of  $t$  in  $\mu$ . If this distribution is not marking dependent, we write  $F_t(\cdot)$ .

Particularly important for continuous-time SPNs is the case where the firing time distributions may depend on the marking only through a “scaling factor” [19]. Define the average firing time of transition  $t$  in marking  $\mu$  as:

$$\forall \mu \in \mathcal{S}_t : f_t(\mu) = \int_0^{\infty} (1 - F_t(\mu, \theta)) d\theta.$$

Then, we require that

$$\forall \mu \in \mathcal{S}_t : F_t(\mu, \theta) = \hat{F}_t\left(\frac{\theta}{f_t(\mu)}\right),$$

where  $\hat{F}_t(\cdot)$  is the “normalized firing time distribution” of  $t$ , which has average one and is not a marking-dependent quantity.

To specify the influence of the firing of a transition on the firing process of other transitions enabled in the current marking, *execution policies* have been introduced in [19]. We allow different execution policies for timed transitions in a SPN which may also depend on the marking [20]. Define  $e_{t,s}(\mu) \in \{R, C\}$  to be the execution policy to be used for transition  $s$  when transition  $t$  fires in marking  $\mu$ . If  $e_{t,s}(\mu) = R$ , transition  $s$  “Restarts” (samples a new random delay from the associated distribution); if  $e_{t,s}(\mu) = C$ , it “Continues”.

### A. Stochastic behavior

The tangible marking  $\mu$  of the SPN as a function of the time  $\theta$  is described by a continuous-time stochastic process, the *marking process*:  $\{\mu\{\theta\}, \theta \geq 0\}$  or by a discrete-time bivariate stochastic process [6]:  $\{(\theta^{[n]}, \mu^{[n]}) : n \in \mathbb{N}\}$ , where  $\theta^{[n]}$  is the instant of time when a timed transition fires and  $\mu^{[n]}$  is marking reached after this firing.  $\theta^{[0]}$  is zero and  $\mu^{[0]}$  is the initial marking.

Consider now the *remaining firing time* (RFT) of each timed transition after a change of the marking. The RFT of transition  $t$  enabled in marking  $\mu^{[n]}$ ,  $\tau_t^{[n]}$ , specifies the time to be spent in markings enabling  $t$  before transition  $t$  can fire. The transition  $t$  with the minimum RFT enabled in  $\mu^{[n]}$  fires at time  $\theta^{[n+1]} = \theta^{[n]} + \tau_t^{[n]}$ . If the firing time distributions of two or more transitions enabled in a marking have jumps at the same instants of time, the probability of them having the same RFT is positive. We do not consider this case, although weights can be used to define a probability mass function over these transitions.

At time  $\theta^{[0]}$ , the RFT of each timed transition enabled in the initial marking is given by a random sample,  $\text{rand}(F_t(\mu^{[0]}, \cdot))$ ,

from the firing time distribution associated with this transition (all other RFTs are undefined). If transition  $t \in \mathbf{E}(\mu^{[n]})$  has the minimum RFT, at time  $\theta^{[n]}$ , the RFT  $\tau_s^{[n+1]}$  of any other transition  $s \in \mathbf{E}(\mu^{[n+1]})$  at time  $\theta^{[n+1]} = \theta^{[n]} + \tau_t^{[n]}$  is:

$$\begin{aligned} \text{rand}(F_s(\mu^{[n+1]}, \cdot)) & \quad \text{if } e_{t,s}(\mu^{[n]}) = R \vee s \notin \mathbf{E}(\mu^{[n]}), \\ (\tau_s^{[n]} - \tau_t^{[n]}) \cdot \frac{f_s(\mu^{[n+1]})}{f_s(\mu^{[n]})} & \quad \text{if } e_{t,s}(\mu^{[n]}) = C \wedge s \in \mathbf{E}(\mu^{[n]}). \end{aligned}$$

Using the terminology of [19], this behavior corresponds to a “race policy”, since the minimum RFT determines the next transition to fire. After the firing of a timed transition, the next tangible marking is reached either directly or after the firing of immediate transitions. The probability of branching to marking  $\nu$  after the firing of timed transition  $t$  in marking  $\mu$  is  $\delta_{\mu,\nu}^t$ .

Furthermore, the definition of  $e$  allows to choose between “age memory”, “enabling memory”, and “resampling” [19] in a marking-dependent way: after the firing of transition  $t$ , a transition  $s$  might either restart,  $e_{t,s} = R$ , or continue,  $e_{t,s} = C$ , its firing time.

The following firing time distributions are important in practical applications:

- *constant*:  $X \sim \text{Const}(c), c \geq 0 \Leftrightarrow \Pr\{X \leq \theta\} = 0$  if  $\theta < c$ , 1 if  $\theta \geq c$ .
- *geometric*:  $X \sim \text{Geom}(p, \sigma), 0 < p \leq 1, \sigma \geq 0 \Leftrightarrow \Pr\{X \leq \theta\} = 1 - (1 - p)^{\lfloor \frac{\theta}{\sigma} \rfloor}$ , where  $\sigma$  is the length of the unit step. The constant distribution is a special case:  $\text{Const}(c)$  is equivalent to  $\text{Geom}(1, c)$ .
- *discrete*:  $X \sim \text{Discr} \Leftrightarrow$  the distribution function of  $X$  is obtained as a weighted sum of a (finite or countably infinite) number of constant distributions. The geometric distribution is a special case. It is possible to approximate any distribution arbitrarily well by using a sufficiently large number of elements in the weighted sum.
- *exponential*:  $X \sim \text{Expo}(\lambda), \lambda > 0 \Leftrightarrow \Pr\{X \leq \theta\} = 1 - e^{-\lambda\theta}$ . This distribution approaches  $\text{Const}(0)$  as  $\lambda$  increases.
- *uniform*:  $X \sim \text{Unif}(a, b), b > a \geq 0 \Leftrightarrow \Pr\{X \leq \theta\} = 0$  if  $\theta < a$ ,  $(\theta - a)/(b - a)$  if  $a \geq \theta \geq b$ , and 1 if  $\theta \geq b$ . This distribution approaches  $\text{Const}(b)$  as  $a$  approaches  $b$ .
- *polynomial*:  $X \sim \text{Poly} \Leftrightarrow$  the distribution function of  $X$  is piecewise defined by polynomials in  $\theta$  (expressions of the form  $\sum_{i=0}^n a_i \theta^i, a_i \in \mathbb{R}$ ) and has finite support  $[\theta_{min}, \theta_{max}]$ . The finite discrete and uniform distributions are special cases. It is possible to approximate any distribution arbitrarily well by using either a sufficiently large number of polynomials of small degree (e.g., constants, as for the discrete distributions) or by using a single polynomial of sufficiently large degree.
- *expolynomial*:  $X \sim \text{Expoly} \Leftrightarrow$  the distribution function of  $X$  is piecewise defined by expolynomials in  $\theta$  (expressions of the form  $\sum_{i=0}^n \sum_{j=0}^m a_{ij} \theta^i e^{-\lambda_{ij}\theta}, a_{ij} \in \mathbb{R}, \lambda_{ij} \in [0, +\infty)$ ). The polynomial and exponential distributions are special cases.

### III. SPNs WITH EFFICIENT SOLUTION

In this section, we describe several types of behavior which might render the solution analytically tractable. This leads to a hierarchy of SPN classes where modeling power is reduced in exchange for an increasingly efficient solution. The classes are defined by the underlying stochastic process.

#### A. Markov SPNs

The main obstacle to an analytical solution is the presence of the RFT in the state description. If the firing time distribution of  $t$  is memoryless, the RFT of  $t$  in  $\mu$  has the same distribution as the entire firing time,  $F_t(\mu, \cdot)$ , hence, there is no need to include it in the state description. Accordingly, two classes of SPNs were defined: we call them “CTMC-SPNs”, where all distributions are exponential [1], [2], and “DTMC-SPNs”, where all distributions are geometric [18], since the marking process  $\{\mu(\theta) : \theta \geq 0\}$  is a continuous-time Markov chain (CTMC) or a discrete-time Markov chain (DTMC), respectively.

As the geometric distribution is memoryless only at discrete time instants multiple of the “time step”  $\sigma$ , exponential and geometric distributions cannot be freely mixed. A special case of memoryless distribution is the constant zero, the distribution of the immediate transitions.

GSPNs [4] are a special case of CTMC-SPNs where the mass at zero is either zero or one. By using state-expansion, any phase-type distribution with any mass at zero still results in an underlying CTMC [19].

The “discrete-time SPNs” defined in [18] allow only geometric distributions with the same step  $\sigma$ , possibly with parameter one, that is, the constant  $\sigma$ , since  $\text{Const}(\sigma)$  is equivalent to  $\text{Geom}(1, \sigma)$ . A discretization analogous to the one used to expand a phase-type distribution can be applied to the discrete-time case [8]. First, a geometric distribution with unit step  $i\sigma$  can be discretized as shown in Figure 1, where  $t_1$  has step 3 and  $t_2$  has step 1. Weights are needed to decide whether transition  $t_1$  or  $t_2$  will fire, given that both attempt to fire, an event which has probability  $pq$  when the underlying DTMC is in state  $(100c)$ . This allows more generality than in [18], since the timing of a transition (i.e.,  $F_{t_1} \sim \text{Geom}(p, 3)$ ) and its ability to fire when competing with other transitions (i.e.,  $w_{t_1} = w_1$ ) are described by different quantities. Then,  $\text{Const}(i\sigma)$  is equivalent to  $\text{Geom}(1, i\sigma)$ , hence TPNs are also reducible to a DTMC with unit step  $\sigma$ , if all constant firing times are a multiple of  $\sigma$ . The process described by a TPN is probabilistic even if its firing times are not random variables since, whenever two transitions have the minimum RFT, the conflict must be resolved probabilistically using the weight information. Finally, since any discrete distribution can be obtained as a weighted combination of constants, any SPN whose firing distributions have as support a subset of  $\{i\sigma : i \in \mathbb{N}\}$  can be reduced to a DTMC with unit step  $\sigma$ .

For both CTMC-SPNs and DTMC-SPNs, steady-state and transient analysis can be performed using standard numerical techniques [6]. Assume that the state space of the process is  $\mathcal{S}$  and the initial probability distribution is  $\pi(0)$ . The steady-state probability vector  $\pi$  of a CTMC described by the infinitesimal generator  $\mathbf{Q}$ , or of a DTMC described by the one-step transition

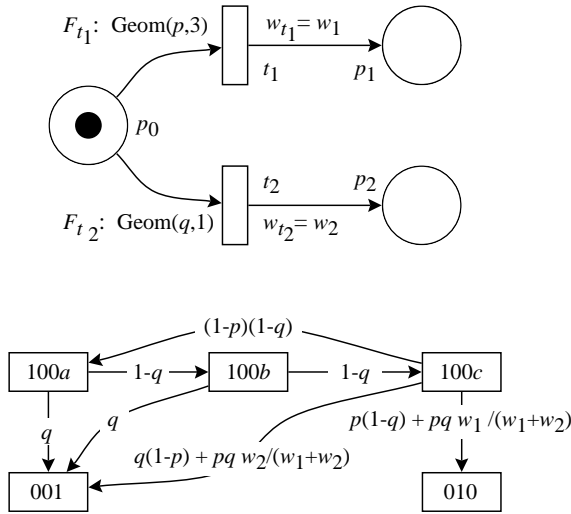


Fig. 1. Discretizing two Geom distributions.

probability matrix  $\mathbf{P}$ , is the solution of

$$\pi \mathbf{Q} = 0 \quad \text{or} \quad \pi(\mathbf{P} - \mathbf{I}) = 0 \quad \text{subject to} \quad \sum_{i \in \mathcal{S}} \pi_i = 1,$$

assuming that  $\mathcal{S}$  contains only one recurrent class of states (if this is not the case,  $\mathcal{S}$  can be partitioned into a transient class and two or more recurrent classes, which can be solved independently). Sparsity-preserving iterative methods such as Gauss-Seidel or Successive Over-Relaxation can be effectively used for the solution. For transient analysis of the continuous case, the transient probability vector at time  $\theta$  is the solution of

$$\frac{d\pi(\theta)}{d\theta} = \pi(\theta)\mathbf{Q} \quad \text{with initial condition} \quad \pi(0)$$

and can be computed using Jensen's method, also called Uniformization or Randomization [21]. For the discrete case, the Power method can be used:

$$\pi((i+1)\sigma) = \pi(i\sigma)\mathbf{P} \quad \text{starting from} \quad \pi(0)$$

(the iterations halt when  $i\sigma \geq \theta$ ). Ergodicity is not required for transient analysis.

### B. Semi-Markov SPNs

If the firing of a transition  $t$  in marking  $\mu^{[n]}$  causes transition  $s$  to restart its firing in  $\mu^{[n+1]}$ ,  $e_{t,s}(\mu^{[n]}) = R$ , the RFT of  $s$  must be resampled in  $\mu^{[n+1]}$ . If all transition pairs behave this way, the marking process is a *semi-Markov process* (SMP), that is, it enjoys absence of memory immediately after every state change [19], [7]. If  $s$  has an exponential distribution, the choice between Restart and Continue is irrelevant and we assume  $e_{t,s} = R$  in this case. The time instants  $\theta^{[n]}$ ,  $n \in \mathbb{N}$  are called *regeneration points* [22].

For transient and steady-state analysis of a SMP, the evolution of the process during the regeneration points must be studied. Equation (1) describes the kernel  $\mathbf{K}(\theta) = [k_{ij}(\theta)]$  of a SMP. Since the future of the marking process after a regeneration point becomes a probabilistic replica of the future of the

process after time zero, if started in the same state, the kernel is also given by Equation (2).

$$k_{ij}(\theta) = \Pr\{\mu^{[n+1]} = j, \theta^{[n+1]} - \theta^{[n]} \leq \theta \mid \mu^{[n]} = i\} \quad (1)$$

$$= \Pr\{\mu^{[1]} = j, \theta^{[1]} \leq \theta \mid \mu^{[0]} = i\}. \quad (2)$$

Equation (3) describes the vector  $\mathbf{h}(\theta) = [h_i(\theta)]$  of holding time distributions in the states of the SMP, which can be reduced to Equation (4).

$$h_i(\theta) = \Pr\{\theta^{[n+1]} - \theta^{[n]} \leq \theta \mid \mu^{[n]} = i\} \quad (3)$$

$$= \Pr\{\theta^{[1]} \leq \theta \mid \mu^{[0]} = i\}. \quad (4)$$

The matrix  $\mathbf{\Pi}(\theta)$  of transient solutions of a SMP is given by the following system of integral equations:

$$\mathbf{\Pi}(\theta) = (\mathbf{I} - \text{diag}(\mathbf{h}(\theta))) + \int_0^\theta \mathbf{\Pi}(\theta - y) d\mathbf{K}(y), \quad (5)$$

where  $\text{diag}(\mathbf{h}(\theta))$  represents a square matrix having the elements of  $\mathbf{h}(\theta)$  on the main diagonal and zeros elsewhere.

For steady-state analysis, an *embedded Markov chain* (EMC) can be defined. The one-step transition probability matrix  $\mathbf{P}$  of the EMC is computed by studying the evolution of the SMP between regeneration points. Having obtained the matrix  $\mathbf{P}$ , the steady-state solution of the EMC can be derived by solving the linear system of global balance equations. Subsequently, the vector  $\mathbf{c}$  of conversion factors is computed. The entries of  $\mathbf{c}$  represent the expected holding times in the states of the SMP between two regeneration points. The solution vector of the EMC is multiplied by the vector  $\mathbf{c}$  and normalized to obtain the steady-state probability vector of the SMP.

The one-step transition probability matrix  $\mathbf{P}$  of the EMC is derived from the kernel:  $\mathbf{P} = \lim_{\theta \rightarrow \infty} \mathbf{K}(\theta)$  and the vector  $\mathbf{c}$  of conversion factors is given by  $\mathbf{c} = \int_0^\infty (1 - \mathbf{h}(\theta)) d\theta$ . The steady-state solution  $\gamma$  of the EMC can be obtained by solving:

$$\gamma \cdot (\mathbf{P} - \mathbf{I}) = \mathbf{0} \quad \text{subject to} \quad \sum_i \gamma_i = 1 \quad (6)$$

and the steady-state solution of the SMP is given by:

$$\pi = \frac{\gamma \cdot \text{diag}(\mathbf{c})}{\gamma \cdot \mathbf{c}}. \quad (7)$$

For a SM-SPN, the entries of kernel and the vector of holding times are given by (for simplicity, we assume that simultaneous firings have zero probability):

$$k_{ij}(\theta) = \sum_{t \in \mathbf{E}(i)} \delta_{ij}^t \cdot \int_0^\theta \prod_{s \in \mathbf{E}(i), s \neq t} (1 - F_s(i, y)) dF_t(i, y),$$

$$h_i(\theta) = 1 - \prod_{t \in \mathbf{E}(i)} (1 - F_t(i, \theta)).$$

Equation (5) can be solved directly or by employing Laplace-Stieltjes transforms as recently proposed in [13], [14]. This solution method may cause numerical difficulties and its computational cost is significant for large models. However, when all firing time distributions are expolynomial distributions, the entries of  $\mathbf{P}$  and  $\mathbf{c}$  can be obtained by symbolic integration, and the steady-state solution can then be obtained by solving (6) and (7).

### C. Semi regenerative SPNs

If there is a marking  $\mu$  and two transitions  $t, s \in \mathbf{E}(\mu)$  such that  $e_{t,s}(\mu) = C$ ,  $t$  can fire before  $s$ , and  $s$  does not have an exponential distribution, the marking process is not semi-Markov. However, under certain conditions, it might be possible to find regeneration points, at which the process enjoys absence of memory. This process is called a *semi regenerative process* (SRP) in [22], so we call *semi regenerative SPN* (SR-SPN) a SPN whose marking process is a SRP. For the transient and steady-state analysis, the evolution of the process between the regeneration points must be studied. Since this can be a GSMP with arbitrarily distributed holding time in each state, the marking process of a SR-SPN is more general than in a MR-SPNs [13] or an extended DSPN [12]. The set of regeneration points of a SR-SPN can be expressed as

$$\{\theta^{[n_k]} : k \in \mathbb{N}, n_k \in \mathbb{N}, n_0 = 0, n_{k+1} > n_k\},$$

where each regeneration point  $\theta^{[n_k]}$  must satisfy the condition that, when the SPN enters marking  $\mu^{[n_k]}$  at time  $\theta^{[n_k]}$  by firing transition  $t$ , any transition enabled in  $\mu^{[n_k]}$  restarts its firing process.

$$\forall \theta^{[n_k]}, \forall s \in \mathbf{E}(\mu^{[n_k]}), e_{t,s}(\mu^{[n_k-1]}) = R.$$

In the following, we concentrate on steady-state analysis. As for SMP, an EMC is defined at regeneration points of a SRP. For the one-step transition probability matrix  $\mathbf{P}$  of the EMC, the evolution of the SRP between the regeneration points must be studied. The steady-state solution of the EMC can be computed as in the case of SMPs, but the conversion factors constitute a matrix rather than a vector. The steady-state probability vector of the SRP is derived by multiplying the steady-state probability vector of the EMC by the matrix of conversion factors and normalizing according to Equations (6) and (8).

The one-step transition probability matrix  $\mathbf{P} = [p_{ij}]$  of the EMC and the matrix  $\mathbf{C} = [c_{ij}]$  of conversion factors are defined by:

$$\begin{aligned} p_{ij} &= \Pr\{\mu^{[n_{k+1}]} = j \mid \mu^{[n_k]} = i\} \\ &= \Pr\{\mu^{[n_1]} = j \mid \mu^{[0]} = i\}, \\ c_{ij} &= \mathbf{E}\{\text{time in } j \text{ during } [\theta^{[n_k]}, \theta^{[n_{k+1}}]) \mid \mu^{[n_k]} = i\} \\ &= \mathbf{E}\{\text{time in } j \text{ during } [0, \theta^{[n_1]}) \mid \mu^{[0]} = i\}. \end{aligned}$$

The steady-state solution of the EMC can still be obtained by solving the linear system of equations (6). The solution of the EMC,  $\gamma$ , is converted to that of the SRP,  $\pi$ , by multiplying by the conversion factors and normalizing:

$$\gamma' = \gamma \cdot \mathbf{C}, \quad \pi = \frac{\gamma'}{\sum_i \gamma'_i} \quad (8)$$

For a constructive definition of SR-SPNs, the sets  $\mathcal{S}_E$ ,  $T_G$ , and  $T_R$ , are introduced [23].  $\mathcal{S}_E$  is the set of all markings in which only exponential transitions are enabled.  $T_G$  is the set of all general (non-exponential) transitions of the SPN.  $T_R \subseteq T_G$  is a set which contains regenerative transitions. A transition  $t \in T_G$  is called regenerative, if all other transitions of the SPN

restart when  $t$  becomes enabled, fires, or becomes disabled. Note that  $T_R$  is not required to contain all general transitions.

*Definition 1—SR-SPN:* A SPN is a SR-SPN, if a set  $T_R$  of regenerative transitions can be found, such that  $\mathcal{S}_E$  and  $\mathcal{S}_t, t \in T_R$  constitute a partition of  $\mathcal{S}$ .

The definition of the regeneration points of a SR-SPN depends on whether a regenerative transition is enabled or not. For states  $\mu^{[n_k]} \in \mathcal{S}_E$ , the next regeneration point is chosen to be the instant of time after the transition with the minimum firing delay has fired:  $\theta^{[n_{k+1}]} = \theta^{[n_k+1]}$ . For states  $\mu^{[n_k]} \in \mathcal{S}_t, t \in T_R$ , the next regeneration point is chosen to be the instant of time after  $t$  has fired or has become disabled.

The possible evolution of the SR-SPN during the enabling period of a regenerative transition  $t$  is described by the *subordinated (stochastic) process* of  $t \in T_R$ . The matrix of transient state probabilities for this process is  $\mathbf{\Pi}_t(\theta) = [\pi_{ij}^t(\theta)]$ :

$$\pi_{ij}^t(\theta) = \Pr\{\text{state } j \text{ at time } \theta \mid \text{state } i \text{ at time } 0\}.$$

Based on  $\mathbf{\Pi}(\theta)$ ,  $\mathbf{P}$  and  $\mathbf{C}$  can be defined row-wise. For all regenerative transitions  $t \in T_R$  the rows corresponding to states  $i \in \mathcal{S}_t$  are defined by:

$$\mathbf{P}_i = \mathbf{u}_i \cdot \mathbf{\Omega}_t \cdot \mathbf{\Delta}_t, \quad (9)$$

$$c_{ij} = \begin{cases} \psi_{ij}^t & \text{if } j \in \mathcal{S}_t \\ 0 & \text{otherwise} \end{cases}, \quad (10)$$

where  $\mathbf{u}_i$  is the  $i$ -th row unity vector,  $\mathbf{\Delta}_t = [\delta_{ij}^t]$  is the matrix of branching probabilities after a firing of  $t$ , and  $\mathbf{\Omega}_t = [\omega_{ij}^t]$  and  $\mathbf{\Psi}_t = [\psi_{ij}^t]$  are the transient probabilities and the expected holding times of the states of the subordinated process:

$$\mathbf{\Omega}_t = \int_0^\infty \mathbf{\Pi}_t(\theta) dF_t(\theta), \quad (11)$$

$$\mathbf{\Psi}_t = \int_0^\infty \mathbf{\Pi}_t(\theta) \cdot (1 - F_t(\theta)) d\theta \quad (12)$$

The entries of  $\mathbf{P}$  and  $\mathbf{C}$  for rows corresponding to states  $i \in \mathcal{S}_E$  are given by

$$p_{ij} = \begin{cases} 0 & \text{if } i = j \\ \frac{\lambda_{ij}}{\lambda_i} & \text{if } i \neq j \end{cases} \quad c_{ij} = \begin{cases} \frac{1}{\lambda_i} & \text{if } i = j \\ 0 & \text{if } i \neq j \end{cases}, \quad (13)$$

where  $\lambda_{ij}$  is the rate leading from state  $i$  to state  $j$  and  $\lambda_i$  is the sum of all outgoing rates for state  $i$ .

If a regenerative transition  $t$  is never enabled together with other transitions, the steady-state solution of a SR-SPN is insensitive to the distribution of  $t$ , since Equations (11) and (12) reduce to:

$$\mathbf{\Omega}_t = \mathbf{I}, \quad \mathbf{\Psi}_t = \text{diag}(f_t(i)).$$

An efficient numerical solution of Equations (11) and (12) is the critical step for the practical application of SR-SPNs. The next section presents a SR-SPN whose subordinated process is a SMP.

The numerical solution of a SR-SPNs with large state space can be performed efficiently if the subordinated processes are CTMCs. In this case, at most one regenerative transition may

be enabled in each marking. SR-SPNs with this restriction are equivalent to the class of extended DSPN defined in [12] and Markov regenerative SPNs defined in [13]. In case of a subordinated CTMC, the matrix of transient state probabilities for the subordinated process is given by the matrix exponential of the generator matrix  $\mathbf{Q}_t$  for the subordinated CTMC of transition  $t$ :

$$\forall t \in T_R : \mathbf{\Pi}_t(\theta) = e^{\mathbf{Q}_t \theta}. \quad (14)$$

In Appendix we show how to generalize Jensen's method for an efficient calculation of the rows of Equations (11) and (12) in case of expolynomial regenerative transitions. This technique has been implemented in TimeNET (Timed Net Evaluation Tool), which can solve SR-SPNs, provided that at most one expolynomial transition is enabled in each marking, plus any number of exponential transitions (TimeNET offers simulation capabilities as well, for SPNs not satisfying this requirement).

The analysis can be generalized to the case where the firing time distribution of a regenerative transition depends on the marking through a scaling factor. This can be done by scaling the generator matrix by the corresponding scaling factors:

$$\hat{\mathbf{Q}}_t = [\hat{q}_{ij}^t] = [f_t(i) \cdot q_{ij}^t]. \quad (15)$$

In this case the matrices  $\mathbf{\Omega}_t$  and  $\mathbf{\Psi}_t$  are given by:

$$\mathbf{\Omega}_t = \int_0^\infty e^{\hat{\mathbf{Q}}_t \theta} d\hat{F}_t(\theta), \quad (16)$$

$$\mathbf{\Psi}_t = \int_0^\infty e^{\hat{\mathbf{Q}}_t \theta} (1 - \hat{F}_t(\theta)) d\theta \cdot \text{diag}(f_t(i)). \quad (17)$$

Equations (16) and (17) generalize the results presented in [24] (see Appendix ).

#### D. Generalized semi-Markov SPNs

If there is a marking  $i$  and two transitions  $t, s \in \mathbf{E}(i)$  such that  $e_{t,s} = e_{s,t} = C$ , and  $t$  and  $s$  do not have an exponentially distributed firing delay, the underlying process is too difficult to study as a SRP, or it might even not be a SRP. The underlying stochastic process is a GSMP. It is also possible to derive the state equations for the transient or steady-state case by means of supplementary variables [12]. The resulting equations constitute a system of partial differential equations which can be analyzed numerically by replacing the differential quotients by finite difference quotients. In practice, however, simulation is the method of choice for the study of large SPNs with generally distributed firing times [15], [17].

Figure 2 summarizes the classes of SPNs and relates them to the underlying stochastic processes.

#### E. Practical limitations

We conclude this section with an informal discussion of the models that can be solved in a reasonable amount of time on a modern workstation. For analytical solutions, the main obstacle is often the memory required to store the reachability graph, or even just its tangible portion. As a rule of thumb,  $10^5$  to  $10^6$  markings and  $10^6$  to  $10^7$  marking-to-marking transitions can be considered the limit. A large amount of virtual memory

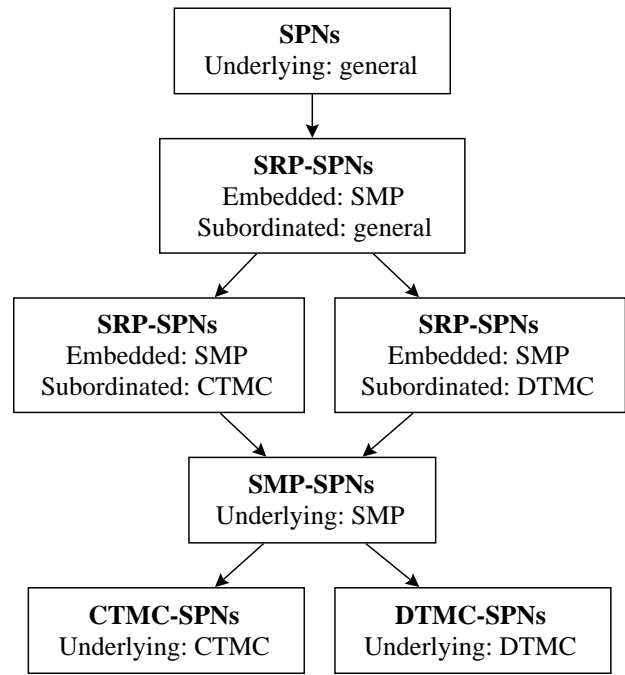


Fig. 2. SPN hierarchy.

is usually required, but it is not in itself sufficient, since the algorithms to build the reachability graph exhibit little locality, causing an excessive number of page faults if not enough main memory is available.

In this respect, the memory requirements for a Markovian SPN (CTMC-SPN or DTMC-SPN) are the most straightforward to understand. For SMP-SPNs, the requirements are similar, since the embedded process is a DTMC. The study of a SR-SPN requires instead to consider multiple stochastic processes. If the regenerative transitions have expolynomial firing distributions and the subordinated processes are CTMCs, it is appropriate to attempt an analytical solution. For the subordinated processes, the memory locality can be higher and the maximum main memory requirements smaller, since the solution of each process is performed in isolation and each of them is usually smaller than the entire chain for a similar Markovian SPN. However, the transition probability matrix describing the embedded process, while possibly being of a smaller dimension than in the Markovian case, often contains many additional entries, corresponding to marking-to-marking *paths*, rather than single transitions. Hence, for SR-SPNs, the overall memory requirements might be better or worse than for a similar Markovian model, depending on the particular model.

Another issue to consider is the execution time required for a steady-state or transient solution. For a Markovian SPN, assuming enough memory is available, the steady-state solution becomes a problem only if the convergence of the linear system is excessively slow. For transient analysis, a large number of iterations is required if the system is stiff, that is, if there is a mixture of slow and fast events (entries differing by many orders of magnitude) and the time at which the solution is required is sufficiently large. For the steady-state study of a SR-SPN, analogous considerations apply to each individual process, since a

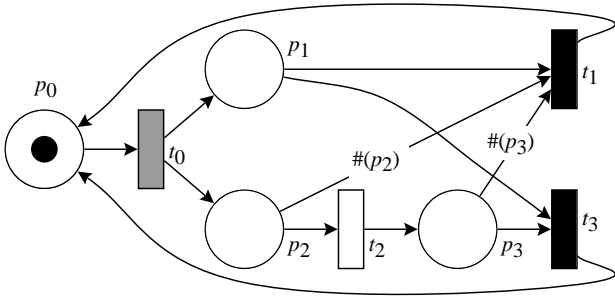


Fig. 3. SR-SPN of a transmission line.

transient analysis of the subordinated processes and a steady-state analysis of the embedded process is required. Hence, the increased generality of the underlying stochastic process does not necessarily have a negative effect on the solvability.

In all cases where a numerical solution is impossible or impractical, such as the analysis of Markovian SPNs with excessively large reachability sets, transient analysis of a non-trivial SMP-SPN or SR-SPN, and analysis of a general SPN or a SR-SPN with non-Markovian subordinated processes, simulation is an effective approach.

#### IV. AN EXAMPLE

In this section, a SPN model of a simple transmission line is considered, to illustrate the steady-state analysis of a SR-SPN. It is assumed that, after the generation of a message, transmission begins and a timeout clock is started. Conflict for the medium can delay the start of transmission. If the timeout elapses before the transmission of the message is completed, the transmission will be repeated.

Figure 3 shows a SPN model of the system. The generation of a message is modeled by transition  $t_0$ , which has an arbitrary firing time distribution with average firing time  $f_{t_0} = \tau_0$ . The timeout and the transmission of the message are represented by transitions  $t_1$  and  $t_3$  with constant firing times of  $\tau_1$  and  $\tau_3$ , respectively. The delay to acquire the medium is modeled by transition  $t_2$ , which has an exponentially distributed firing time with rate  $\lambda$ . The multiplicity of some input arcs is marking-dependent to ensure that places  $p_1$ ,  $p_2$ , and  $p_3$  are empty after the firing of  $t_1$  or  $t_3$ . If the timeout is not larger than the transmission time, no successful transmission can ever take place, hence we assume  $\tau_1 > \tau_3$ .

In this SPN,  $t_1$  and  $t_3$  have constant firing times, are concurrently enabled, and start their firing process at different instants of time. Nevertheless, the analysis is possible using firings of the transitions  $t_0$  and  $t_1$  as regeneration points:  $T_R = \{t_0, t_1\}$ . The reachability set of the SR-SPN consists of three markings and is shown in Figure 4:

$$\mathcal{S} = \{0, 1, 2\}, \quad 0 : [1, 0, 0, 0], \quad 1 : [0, 1, 1, 0], \quad 2 : [0, 1, 0, 1].$$

The sets  $\mathcal{S}_{t_0} = \{0\}$  and  $\mathcal{S}_{t_1} = \{1, 2\}$  constitute a partition of the reachability set  $\mathcal{S}$ . Transition  $t_0$  is exclusively enabled, hence the steady-state solution of the SPN is insensitive to the distribution of  $t_0$ , it only depends on the average firing time

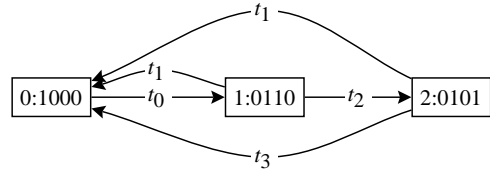
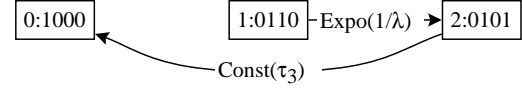


Fig. 4. The reachability graph for the model.

Fig. 5. The SMP subordinated to  $t_1$ .

$\tau_0$ . The process subordinated to transition  $t_1$  is a SMP and is shown in Figure 5. Since  $t_1$  can become enabled only upon entering marking 1, the first and last row of  $\Pi_{t_1}(\theta)$ ,  $\Omega_{t_1}$ , and  $\Psi_{t_1}$  are not needed. Since neither  $t_0$  nor  $t_1$  can become enabled upon entering marking 2, the last row of  $\mathbf{C}$  is not needed either. In addition, after  $t_1$  fires, the SPN cannot be in marking 2, so the last column and row of  $\mathbf{P}$  are not needed either. In other words,  $\mathbf{P}$  only needs to describe the probability of transitions between markings 0 and 1. Finally, entry  $\psi_{1,0}^{t_1}$  does not need to be computed because transition  $t_1$  is not enabled in marking 0. For simplicity, we denote unneeded entries with the symbol “-”.

The matrix  $\Pi_{t_1}(\theta)$  of the transient state probabilities for the SMP subordinated to  $t_1$  can be obtained symbolically:

$$\Pi_{t_1}(\theta) = [\pi_{ij}^{t_1}] = \begin{bmatrix} - & - & - \\ 1 - e^{-\lambda(\theta - \min(\theta, \tau_3))} & e^{-\lambda\theta} & e^{-\lambda(\theta - \min(\theta, \tau_3))} - e^{-\lambda\theta} \\ - & - & - \end{bmatrix}.$$

The matrices of state probabilities of the SMP at the instant of firing of  $t_1$ ,  $\Omega_{t_1}$ , and of expected holding times in each marking up to the firing of  $t_1$ ,  $\Psi_{t_1}$ , are:

$$\Omega_{t_1} = [\omega_{ij}^{t_1}] = \int_0^\infty \Pi_{t_1}(\theta) du(\theta - \tau_1) = \Pi_{t_1}(\tau_1) = \begin{bmatrix} - & - & - \\ 1 - e^{-\lambda(\tau_1 - \tau_3)} & e^{-\lambda\tau_1} & e^{-\lambda(\tau_1 - \tau_3)} - e^{-\lambda\tau_1} \\ - & - & - \end{bmatrix}$$

and

$$\Psi_{t_1} = [\psi_{ij}^{t_1}] = \int_0^\infty \Pi_{t_1}(\theta)(1 - u(\theta - \tau_1))d\theta = \int_0^{\tau_1} \Pi_{t_1}(\theta)d\theta = \begin{bmatrix} - & - & - \\ - & \frac{1 - e^{-\lambda\tau_1}}{\lambda} & \tau_3 - \frac{e^{-\lambda\tau_1}(e^{\lambda\tau_3} - 1)}{\lambda} \\ - & - & - \end{bmatrix},$$

where  $u(\cdot)$  is the unit step function. Employing Equations (9) and (10) yields the one-step transition probability matrix  $\mathbf{P}$  of the EMC and the matrix of conversion factors  $\mathbf{C}$ :

$$\mathbf{P} = \begin{bmatrix} 0 & 1 & - \\ 1 & 0 & - \\ - & - & - \end{bmatrix}, \quad \mathbf{C} = \begin{bmatrix} \tau_0 & 0 & 0 \\ 0 & \psi_{11}^{t_1} & \psi_{12}^{t_1} \\ - & - & - \end{bmatrix}.$$

All changes of marking caused by firings of transition  $t_1$  lead to marking 0. The steady-state probability vector of the EMC is computed by solving the linear system of equations (6). In this particular case, the solution is:

$$\gamma = \begin{bmatrix} \frac{1}{2} & \frac{1}{2} & - \end{bmatrix}.$$

The steady-state marking probability vector  $\pi$  of the SR-SPN is obtained as the product of the steady-state probability vector of the EMC by the matrix  $\mathbf{C}$  of conversion factors:

$$\begin{aligned} \gamma' &= \begin{bmatrix} \frac{\tau_0}{2} & \frac{\psi_{11}^{t_1}}{2} & \frac{\psi_{12}^{t_1}}{2} \end{bmatrix} \\ &= \begin{bmatrix} \frac{\tau_0}{2} & \frac{1 - e^{-\lambda\tau_1}}{2\lambda} & \frac{\tau_3}{2} - \frac{e^{-\lambda\tau_1}(e^{\lambda\tau_3} - 1)}{2\lambda} \end{bmatrix} \end{aligned}$$

and by subsequently normalizing  $\gamma'$  according to Equation (8).

For a numerical example, assume  $\tau_0 = 1$ ,  $\tau_1 = 5$ ,  $\lambda = 0.5$ ,  $\tau_3 = 1$ . Then

$$[\omega_{10}^{t_1} \ \omega_{11}^{t_1} \ \omega_{12}^{t_1}] = [0.864665 \ 0.082085 \ 0.053250],$$

$$[- \ \psi_{11}^{t_1} \ \psi_{12}^{t_1}] = [- \ 1.83583 \ 0.893499],$$

and

$$\pi = [0.268145 \ 0.492268 \ 0.239587].$$

The average cycle time for the token is given by the sum of the average enabling times for  $t_0$ ,  $\tau_0$ , and  $t_1$ ,  $\psi_{11}^{t_1} + \psi_{12}^{t_1}$ :

$$\tau_0 + (\psi_{11}^{t_1} + \psi_{12}^{t_1}) = 3.72933,$$

and its throughput is

$$\frac{1}{3.7293294} = 0.268145.$$

However, only a portion  $\omega_{10}^{t_1}$  of this throughput corresponds to successful completions of the transmission, hence the real transmission throughput is

$$0.268145 \cdot 0.864665 = 0.231856.$$

Finally, when a timeout occurs, the probability that the transmission has not yet started is

$$\frac{\omega_{11}^{t_1}}{1 - \omega_{10}^{t_1}} = 0.606531.$$

The complementary probability,

$$\frac{\omega_{12}^{t_1}}{1 - \omega_{10}^{t_1}} = 0.393469,$$

corresponds to the undesirable event of having a timeout while the transmission is underway.

## CONCLUSION

In this paper, we have classified the SPNs into various classes, according to the nature of their underlying stochastic process. The most complex class we identified, SR-SPNs, corresponds to semi-regenerative processes and effectively extends the class of SPNs for which an analytical solution is known.

We illustrate the type of behavior that can be modeled by the SR-SPNs using a simple system transmitting messages as an example. In it, two deterministic transitions can become enabled concurrently, but not necessarily at the same time. A similar model was given as an example of a DSPN which cannot be solved with previously known methods [9].

## APPENDIX

In this appendix we derive an efficient numerical computation of Equations (11) and (12) for a transition  $t$  with an exponential distributed firing time and a subordinated CTMC [23]. The presented formulas generalize Jensen's method and the formulas presented in [12] for polynomial distributions.

For  $\theta \in (0, \infty)$ ,  $m \in \mathbb{N}$ ,  $\lambda \in [0, \infty)$ , define

$$\mathbf{E}^{(\theta)} = e^{\mathbf{Q}\theta}, \quad \mathbf{L}^{(\theta, m, \lambda)} = \int_0^\theta y^m e^{-\lambda y} e^{\mathbf{Q}y} dy$$

The solution of (11) and (12) is a weighted sum of matrices  $\mathbf{E}^{(\theta)}$  and  $\mathbf{L}^{(\theta, m, \lambda)}$ .  $\mathbf{E}^{(\theta)}$  can be calculated with Jensen's method: define

$$\mathbf{A} = \frac{1}{q} \mathbf{Q} + \mathbf{I}, \quad q = 1.02 \cdot \max_i |q_{ii}|$$

The rows of  $\mathbf{E}^{(\theta)}$  are obtained as

$$\mathbf{E}^{(\theta)}(i) \approx \sum_{k=L}^R \Phi(k) \cdot \beta(k, q\theta)$$

where  $\Phi$  is calculated by iterative vector-matrix multiplications:

$$\Phi(0) = \mathbf{u}_i, \quad \Phi(k+1) = \Phi(k) \cdot \mathbf{A}$$

$\mathbf{u}_i$  is the  $i$ -th row unity-vector and  $\beta(k, q\theta)$  is the  $k$ -th Poisson probability in  $q\theta$  which can be calculated iteratively by:

$$\beta(0, q\theta) = e^{-q\theta}, \quad \beta(k+1, q\theta) = \beta(k, q\theta) \cdot \frac{q\theta}{k+1}$$

The truncation points  $L$  and  $R$  of the summation can be estimated for a given error tolerance [6].

For the calculation of  $\mathbf{L}^{(\theta, m, \lambda)}$ , the power series of the matrix exponential can be substituted:

$$\begin{aligned} \mathbf{L}^{(\theta, m, \lambda)} &= \int_0^\theta y^m \cdot e^{-\lambda y} \cdot \left( \sum_{k=0}^{\infty} \mathbf{A}^k \cdot \beta(k, qy) \right) dy \\ &= \sum_{k=0}^{\infty} \mathbf{A}^k \frac{(k+m)! q^k}{k! (q+\lambda)^{k+m+1}} \left( 1 - \sum_{h=0}^{k+m} \beta(h, (q+\lambda)\theta) \right) \end{aligned}$$

Applying right truncation leads to:

$$\mathbf{L}^{(\theta, m, \lambda)}(i) \approx \sum_{k=0}^R \Phi(k) \cdot \gamma(k) \cdot \eta(k)$$

where  $\gamma(k)$  and  $\eta(k)$  are calculated iteratively:

$$\gamma(0) = \frac{m!}{(q+\lambda)^{m+1}}, \quad \gamma(k+1) = \gamma(k) \cdot \frac{k+m+1}{k+1} \cdot \frac{q}{q+\lambda}$$

$$\eta(0) = 1 - \sum_{h=0}^m \beta(h, (q+\lambda)\theta)$$

$$\eta(k+1) = \eta(k) - \beta(k+m+1, (q+\lambda)\theta)$$

A criterion to bound the truncation error can be derived. The entries of each row of the matrix exponential sum to one. The truncation error of each entry of  $\mathbf{L}^{(\theta, m, \lambda)}$  is bounded by  $\varepsilon$ , if  $R$  satisfies

$$R = \min_{r \in \mathbb{N}} \left\{ s - \sum_{h=0}^r \gamma(h)\eta(h) \leq \varepsilon \right\}$$

where  $s$  is the (exact) sum of each row of  $\mathbf{L}^{(\theta, m, \lambda)}$ . If  $\lambda = 0$ ,  $s$  is given by

$$s = \int_0^\theta y^m dy = \frac{\theta^{m+1}}{m+1}$$

If  $\lambda > 0$ ,  $s$  is given by

$$s = \int_0^\theta y^m e^{-\lambda y} dy = \frac{m!}{\lambda^{m+1}} \cdot \left( 1 - \sum_{h=0}^m \beta(h, \lambda\theta) \right)$$

The computational effort for the calculation of one row of  $\mathbf{L}^{(\theta, m, \lambda)}$  depends mainly on the number of vector-matrix multiplications. If a weighted sum of matrices  $\mathbf{E}^{(\theta)}$  and  $\mathbf{L}^{(\theta, m, \lambda)}$  is required, it is possible to factor out the matrix powers, thus avoiding repeated vector-matrix multiplications. The asymptotical complexity for the numerical solution in case of an exponential distribution is therefore of the same order as in the case of a deterministic firing time.

In this appendix we derive Equations (16) and (17) presented for regenerative SPNs with a transition  $t$  with a general distributed firing time depending on the marking through a scaling factor and with a subordinated CTMC. Define the normalized state probabilities of the subordinated CTMC as  $(\theta_j)$  is the absolute and  $\hat{\theta}$  is the normalized elapsed firing time of  $t$ ):

$$\hat{\pi}_{ij}^t(\hat{\theta}) = \pi_{ij}^t(f_t(j) \cdot \hat{\theta}) = \pi_{ij}^t(\theta_j)$$

The matrix of normalized state probabilities is given by the matrix exponential of the scaled generator matrix  $\hat{\mathbf{Q}}$  (this can be shown by the underlying system of differential equations [24]):

$$\hat{\mathbf{\Pi}}_t(\hat{\theta}) = \left[ \hat{\pi}_{ij}^t(\hat{\theta}) \right] = e^{\hat{\mathbf{Q}}\hat{\theta}}$$

Define  $\omega_{ij}^t$  as the probability, that the subordinated CTMC is in state  $j$  after  $t$  fires, given it was in state  $i$  initially, and  $\psi_{ij}^t$  as the expected holding time in state  $j$  up to the firing of  $t$ . Integrating by substitution:

$$\omega_{ij}^t = \int_0^\infty \pi_{ij}^t(\theta_j) dF_t(j, \theta_j) = \int_0^\infty \hat{\pi}_{ij}^t(\hat{\theta}) d\hat{F}_t(\hat{\theta})$$

$$\psi_{ij}^t = \int_0^\infty \pi_{ij}^t(\theta_j) (1 - F_t(j, \theta_j)) d\theta_j$$

$$= \int_0^\infty \hat{\pi}_{ij}^t(\hat{\theta}) (1 - \hat{F}_t(\hat{\theta})) f_t(j) d\hat{\theta}$$

Substitution of the entries of the matrix exponential leads to Equations (16) and (17).

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